

NON-STORMWATER INFORMATION PACKAGE

CONTRACT NO. 04-165421

04-ALA-880-KP 43.6/45.5

**IN ALAMEDA COUNTY HIGH STREET OVERHEAD SEISMIC RETROFIT
BRIDGE #33-0732 L/R (HIGH STREET SEPARATION & OH) AND BRIDGE
#33-0681 S (ROUTE 880 ON-RAMP OC) LOCATED ON I-880**

California Department of Transportation
District 4
Water Quality Program
111 Grand Avenue
Oakland, California 94612

March 2008

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CONTRACT NO. 04-165421

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1. ESTIMATE RATE OF SEEPAGE

Rec'd 4/11/08
Business, Transportation and Housing Agency

Memorandum

*Flex your power!
Be energy efficient!*

To: MR. JERRY MA
District Office Chief
Office of Design Alameda I

Attention: Albert Zepeda

Date: March 28, 2008

File: 4-Ala-880 KP 43.6/45.5
4-165421
High St. Viaduct

From: WAJAHAT NYAZ
Chief, Branch C
Office of Geotechnical Design – West
Geotechnical Services
Division of Engineering Services

Subject: Estimate of Seepage Flow Rate for Excavations

Per your request, we are providing an estimate for the groundwater seepage flow rate expected during the excavations for this project. Based on the project plans and results of our subsurface investigation, we estimate that dewatering will be required at Bents 2-9, Bents 10-12 for the High Street Viaduct and the proposed pump plant . It is our understanding that this “flow rate” will be included in the dewatering specifications to allow the contractor to estimate the amount of dewatering required for this project.

The flow of groundwater through porous media, such as soil, is dependent upon many variables. The most important parameters that control the flow of water in soil are the permeability of the soil and the head differential. The permeability of the soil can be determined from laboratory test results or a site pump test. In the absence of laboratory tests or pump test data, an estimate of the permeability can be made based on standard correlations published in geotechnical literature. Head differential can be determined based on the elevation of the measured phreatic surface and the anticipated drawdown needed to keep the ground surface dry and workable.

The permeability of soil is generally very difficult to estimate accurately from laboratory tests and correlations. This is because the permeability of the soil is dependent on numerous factors such as the soil density, the void ratio, the presence of sand or silt lenses, the soil saturation, sample disturbance, etc. It is virtually impossible to account for all these factors accurately in the laboratory or when correlating with published values. Consequently, permeability based on laboratory tests and /or correlations can be

MR. JERRY MA
Attn: A. Zepeda
March 28, 2008
Page 2

off by orders of magnitude. For this project, we estimated the seepage using soil description and published soil data correlations.

The estimated seepage flow rate is approximately as follows:

High Viaduct Bents 2-9: 0.003 cubic meter/day/sq meter (0.01 cubic feet/day/sq ft)
High Viaduct Bents 10-12: 0.044 cubic meter/day/sq meter (0.143 cubic feet/day/sq ft)
Pumping Plant: 0.003 cubic meter/day/sq meter (0.01 cubic feet/day/sq ft)

Please send the dewatering specification for our review.

If you have any questions, please contact Wajahat Nyaz at 510-622-1777.

c: WNyaz, TPokrywka, BLee, Daily File, Route File, TransLab

BLee/mm

11/29/07
FCC/Al
A2
CJA/mad

Cat 313 Geotech
ASA Groundwater

Flex your power!
Be energy efficient!

Memorandum

To: MR. JERRY MA
District Office Chief
Office of Design Alameda I

Date: November 27, 2007

Attention: Albert Zepeda

File: 4-Ala-880 KP 43.6/45.5
4-165421
High St. Viaduct

From: BETTY LEE
Associate M & R Engineer
Office of Geotechnical Design – West
Geotechnical Services
Division of Engineering Services

WAJAHAT NYAZ
Chief, Branch C
Office of Geotechnical Design – West
Geotechnical Services
Division of Engineering Services

Subject: Archeology Site—Groundwater Control

Per your request, we did an assessment of groundwater impact/mitigation measure on the proposed archeological study site at the vicinity of S Line, Sta. 503+40 to 504+00. Since your request was made after the completion of borehole drilling and Geotechnical Design Report, this assessment was made based on existing available subsurface data, namely, data of Boreholes B1, B2 and M2. These boreholes are the nearest available boreholes to the proposed archeological site. The actual subsurface condition may vary.

Since the Contractor will be responsible for the design of the shoring and dewatering of the site, it is up to the Contractor to decide what dewatering method to use. This memo is for estimating purpose only.

According to Thad Van Bueren of Archeology, an initial excavation of 4 ft. deep will be made. Subsequent hand-excavations of 5-6 ft. deep will be made at locations with discovered features; in addition, as many as two deeper features of up to 12 ft. below the initial excavation floor will be made.

Based on the existing boreholes, the subsurface consists mainly of lean clay and sandy lean clay (CL), with the exception of a 1 m thick layer of dense clayey gravel (GC) at elevation 2 m, underlain by a 3 m thick layer of medium dense clayey sand (SC) found in Borehole B2. On May 14, 2002, groundwater level was at Elevation 0.2 m, approximately 1 m above the bottom of the proposed excavation (of the deepest feature).

MR. JERRY MA

Attn: A. Zepeda

November 27, 2007

Page 2

Based on the above subsurface conditions, a likely method of groundwater control is the use of sheet piling cutoff walls and sump pumping. The estimated seepage flow is approximately 0.01 gpm/ sq ft of wall per foot of differential head. (Reference: NAVFAV DM-7.2, May 1982)

If you have any questions, please call Betty Lee at (510) 286-4825 or Wajahat Nyaz at (510) 622-1777.

c: WNyaz, TPokrywka, BLee, Daily File, Route File

BLee/mm

2. SITE INVESTIGATION REPORT-GROUNDWATER MONITORING
RESULTS

EXECUTIVE SUMMARY

This Site Investigation Report was prepared for the State Route (SR) 880, High Street Overcrossing Project. The investigation was performed underneath SR 880 from Kilometer Post (KP) 43.5 to KP 45.5, in the city of Oakland, California. The Site location is depicted on the Vicinity Map, Figure 1.

The primary objectives of the scope of services were to: 1) evaluate whether impacts due to aerially deposited lead (ADL) exist in the surface soil within the project boundaries; and 2) evaluate whether impacts due to petroleum hydrocarbons exist in the groundwater under the subject site. The information obtained from this investigation will be used by Caltrans to coordinate overhead replacement activities, determine soil disposal costs, and identify health and safety concerns during improvements.

The field investigation was performed on May 24, 26, 27 & 31, 2005. The following field activities were performed during soil sampling efforts.

- Advanced 20 soil borings using a hand auger to safely avoid underground utilities, and completed sampling with a direct push rig.
- Further advanced 10 borings for groundwater sampling using direct push rig method.
- Collected samples in pre-cleaned and unused glass jars.
- Transported samples to a California-certified environmental laboratory.

Soil samples were collected from 20 borings where overcrossing replacement activities are planned. Boring locations are shown on the Site Plans, Figures 2 through 5. Boring locations were surveyed using Differential Global Positioning System (DGPS) equipment. Boring coordinates are presented in Table 1.

Soil borings were advanced to a depth of approximately 0.75 meter (2.5 feet) below ground surface (bgs) using hand augers and a direct push rig. (For safety, the hand auger was used from the surface to below the typical depth of underground utilities. From that point, the direct push rig continued with the sampling.) Ten borings were advanced further with the direct push rig to approximately 8 meters (26 feet) bgs for the purpose of collecting grab-groundwater samples. Select soil boring logs are included as Appendix A.

Soil samples were collected from each boring location at an approximate depth of 0 to 0.15 meters (0 to 0.5 foot), 0.3 to 0.45 meters (1 to 1.5 feet), and 0.6 to 0.75 meters (2 to 2.5 feet). A total of 60 soil samples were collected. Completed soil boreholes were backfilled to surface with the soil cuttings. Groundwater was not encountered during the advancement of the boreholes.

The laboratory testing performed for soil samples is summarized below:

- Sixty soil samples were analyzed for total lead using EPA Test Method 6010B.
- Six soil samples were analyzed for pH using EPA Test Method 9045C.
- Twenty-nine soil samples with total lead concentrations greater than 50 milligrams per kilogram (mg/kg) were further analyzed for soluble lead using the Waste Extraction Test (WET).
- Thirty soil samples were further analyzed for soluble lead using the Toxicity Characteristic Leaching Procedure (TCLP).

All groundwater samples were analyzed for the following:

- TPHg, TPHd, and TPHmo using EPA Test Method 8015b.
- SVOCs using EPA Test Method 8270c.
- VOCs using EPA Test Method 8260b

Additionally, two trip blank samples were analyzed for VOCs and two equipment rinse-blank samples were analyzed for lead.

Laboratory analyses were performed under standard, one week turn-around-time. A summary of the analytical laboratory test results for lead and pH is presented as Table 2. Reproductions of the laboratory reports and chain-of-custody documentation are presented as Appendix A.

The laboratory analyses indicated the following:

- Reported total lead concentrations in soil ranged from <0.5 mg/kg to 1,600 mg/kg.
- Soil samples analyzed using the WET method exhibited concentrations ranging from 0.63 mg/L to 48 mg/L.
- Soil samples analyzed for soluble (TCLP) lead exhibited concentrations between <0.25 mg/L and 15 mg/L.
- Soil pH values ranged from 7.79 to 8.45.
- Lead was not detected in the equipment rinse blanks.
- TPHg was detected in one grab groundwater sample, at a concentration of 0.19 mg/L.
- TPHd was reported in most grab groundwater samples, at concentrations ranging from less than the laboratory reporting limit of 0.056 mg/L to 0.15 mg/L.
- TPHmo was reported in most grab groundwater samples, at concentrations ranging from less than the laboratory reporting limit of 0.056 mg/L to 0.22mg/L.
- The only VOCs detected in grab-groundwater were Ethylbenzene (0.89 ug/L), Xylenes (2.3 ug/L), and Toluene (14 ug/L) in B5S and Trichloroethene (4.6 ug/L) in B9S.
- SVOCs were not detected in grab-groundwater samples above laboratory reporting limits.

The non-parametric standard bootstrap method was applied to the total lead data to evaluate the upper confidence limits (UCLs) of the true means of the total lead concentrations for each sampling depth. Where lead was not detected, one-half the laboratory reporting limit value was used in the UCL calculations. UCLs could not be calculated for those locations with three or fewer boring and the maximum detected concentrations were used as representative.

Summarized in the following table are the total lead representative concentrations and predicted soluble (WET) lead concentrations. In addition, soil reuse and disposal options are evaluated.

Borings south of High Street

Excavation Scenario	Onsite Reuse		Offsite Disposal	
	90% UCL (mg/kg)	Predicted WET Lead (mg/L)	95% UCL (mg/kg)	Predicted WET Lead (mg/L)
Surface to 0.3 meter (0 to 1 ft)	585	58.2	641	63.8
<i>Underlying soil (0.3 to 0.75 meter)</i>	183	18.2	198	19.7
Surface to 0.6 meter (0 to 2 ft)	389	38.8	426	42.4
<i>Underlying soil (0.6 to 0.75 meter)</i>	160	16.0	171	17.1
Surface to 0.75 meter (0 to 2.5 ft)	344	34.2	375	37.3

Based on the above table, soil generated from all excavation scenarios in this area will be classified as a California hazardous waste since the predicted soluble (WET) lead concentrations are greater than the STLC value of 5 mg/L. Soil generated for offsite disposal must be disposed at a Class 1 facility. Based on the soluble (TCLP) results and regression analysis, excavated soil would not be classified as RCRA hazardous (see Appendix C).

Borings between High Street and 42nd Avenue ramps

Excavation Scenario	Onsite Reuse		Offsite Disposal	
	90% UCL (mg/kg)	Predicted WET Lead (mg/L)	95% UCL (mg/kg)	Predicted WET Lead (mg/L)
Surface to 0.3 meter (0 to 1 ft)	259	25.8	270	26.9
<i>Underlying soil (0.3 to 0.75 meter)</i>	173	17.2	191	19.0
Surface to 0.6 meter (0 to 2 ft)	252	25.1	271	27.0
<i>Underlying soil (0.6 to 0.75 meter)</i>	26	2.6	28	2.8
Surface to 0.75 meter (0 to 2.5 ft)	207	20.6	223	22.2

Based on the above table, soil generated from ground surface to 0.6 meter (2 feet) in depth will be classified as a California hazardous waste since the predicted soluble (WET) lead concentrations are greater than the STLC value of 5 mg/L. Soil generated for offsite disposal from excavations to 0.6 meter (2 feet) bgs must be disposed at a Class 1 facility. Underlying soil (i.e., deeper than 0.6 meter bgs) will not be classified as a hazardous waste. Based on the soluble (TCLP) results and regression analysis, excavated soil would not be classified as RCRA hazardous (see Appendix C).

Borings north of 42nd Avenue ramps

Excavation Scenario	Onsite Reuse		Offsite Disposal	
	90% UCL (mg/kg)	Predicted WET Lead (mg/L)	95% UCL (mg/kg)	Predicted WET Lead (mg/L)
Surface to 0.3 meter (0 to 1 ft)	562	56.0	589	58.6
<i>Underlying soil (0.3 to 0.75 meter)</i>	58	5.7	62	6.2
Surface to 0.6 meter (0 to 2 ft)	321	32.0	338	33.6
<i>Underlying soil (0.6 to 0.75 meter)</i>	13	1.3	13	1.3
Surface to 0.75 meter (0 to 2.5 ft)	259	25.8	273	27.2

Based on the above table, soil generated from ground surface to 0.6 meter (2 feet) in depth will be classified as a California hazardous waste since the predicted soluble (WET) lead concentrations are greater than the STLC value of 5 mg/L. Soil generated for offsite disposal from excavations to 0.6 meter (2 feet) bgs must be disposed at a Class 1 facility. Underlying soil (i.e., deeper than 0.6 meter bgs) will not be classified as a hazardous waste. Based on the soluble (TCLP) results and regression analysis, excavated soil would not be classified as RCRA hazardous (see Appendix C).

Groundwater analytical results were compared with the Environmental Screening Levels (ESLs) for Estuarine Habitats, established by the San Francisco Bay Regional Water Quality Control Board (SF-RWQCB), to assess whether further action may be needed. ESLs are considered to be conservative and under most circumstances concentrations below ESLs can be assumed to not pose a significant threat to human health and the environment. None of the contaminants detected exceeded their respective ESL for Estuarine habitats.

The soil sample results were compared to SF-RWQCB ESLs for shallow soil under an industrial/commercial land use. ESLs are considered to be conservative and under most circumstances, concentrations below ESLs can be assumed to not pose a significant threat to human health and the environment. The highest UCL of 585 mg/kg is less than shallow soil ESL of 750 mg/kg for lead in shallow soil. Therefore, it is concluded that risk to the health of workers performing the construction activities due to lead-impacted soil in the areas investigated is minimal.

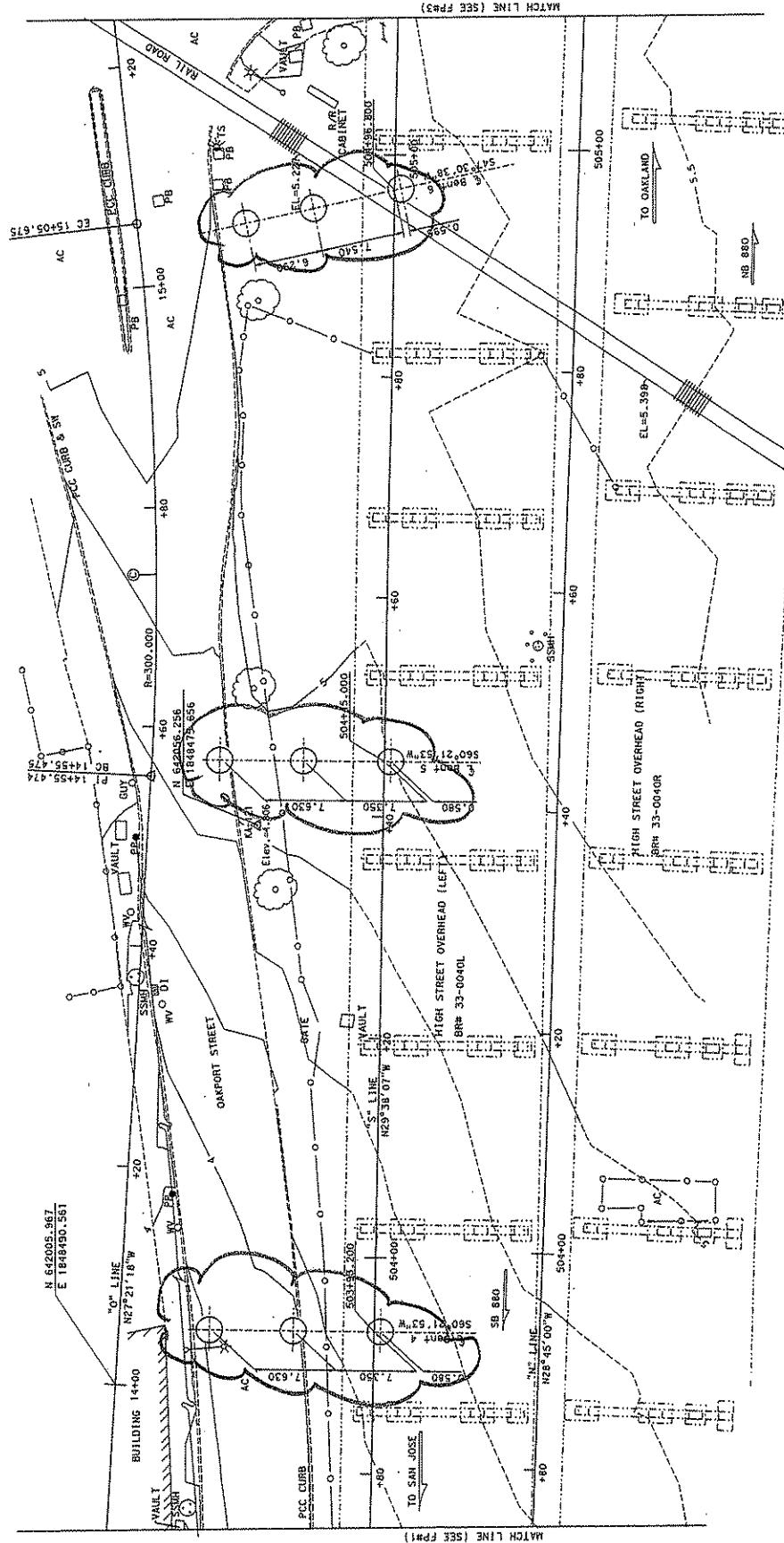
3. DEWATERING LOCATION PLANS



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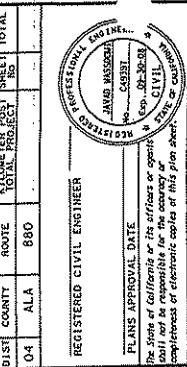


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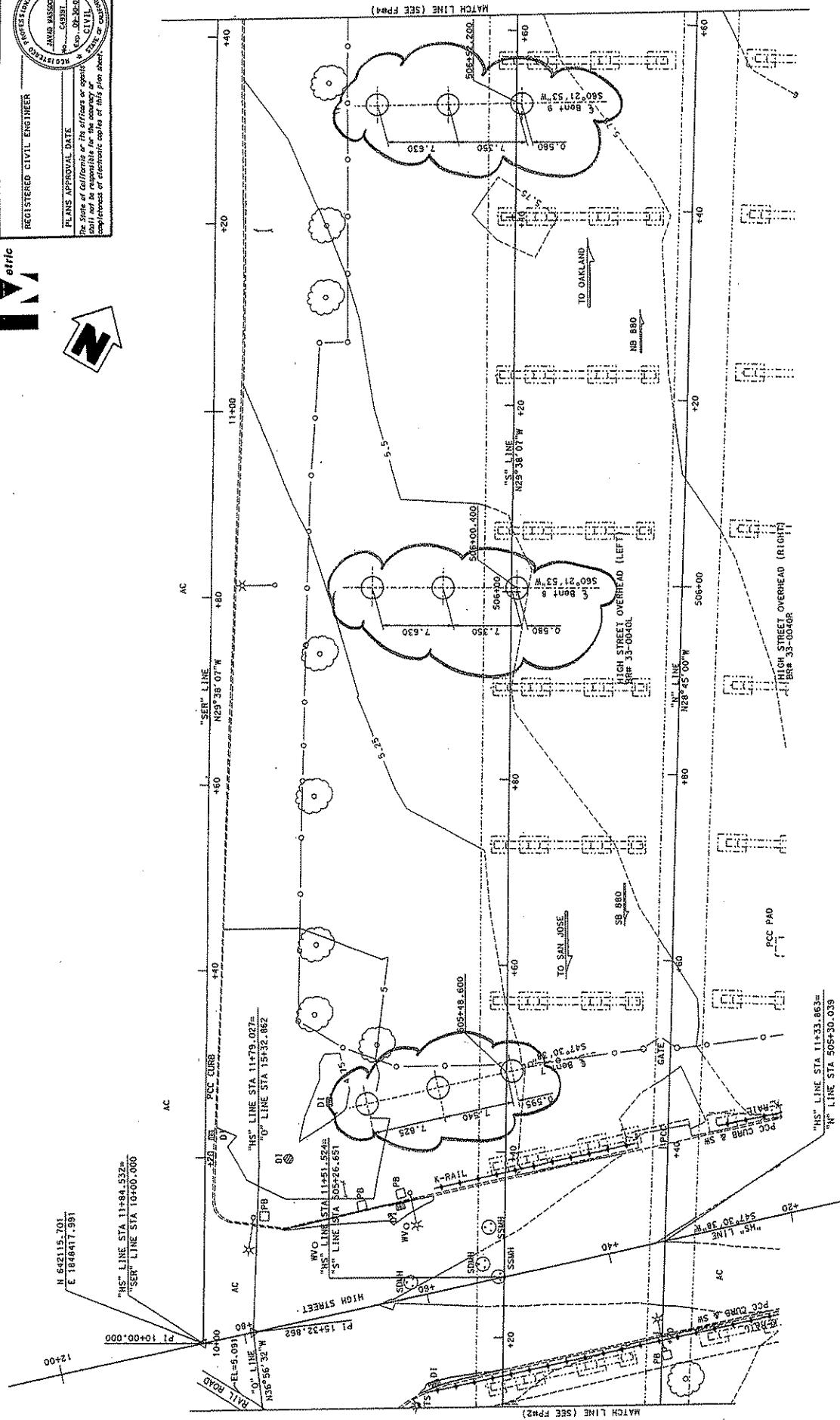


ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

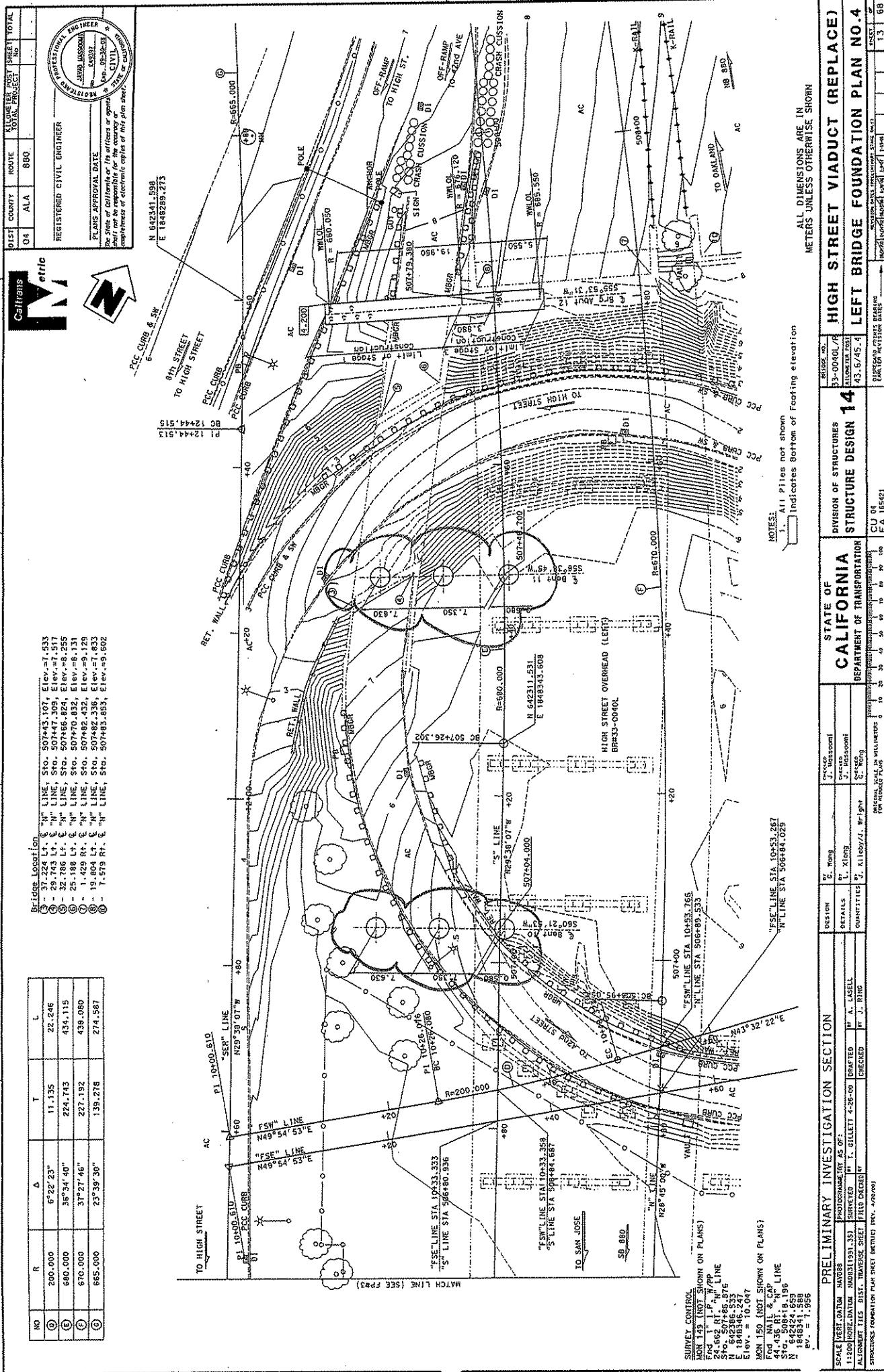
HIGH STREET VIADUCT (REPLACE)



"H5" LINE STA 11+84.532=



ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN



No	R	A	T	L
⑤	1790.000	4°12'41"	65.814	131.569

RHOL
R# 1809.950
3.575

SB 8100
502+55.300
WHLOL
H28°45'00" W



DIST	COUNTY	ROUTE	LIGHTING TEST	STREET TOTAL
04	ALA	880		

REGISTERED CIVIL ENGINEER
PLANS APPROVAL DATE
The State of California or its officers or agents
shall not be responsible for the accuracy of
any components or electronic copies of this plan sheet or quantity
plan sheet.



REGISTRATION NO.
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CITY
STATE
EXPIRATION DATE

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H 642056.256

Detailed description of the site plan:

- High Street Overhead (Left):** Located at ELEV. 44.806, spanning 33'-04".
- High Street Overhead (Right):** Located at ELEV. 44.800, spanning 33'-04".
- PCC Curb:** Located along the bottom edge of the plan.
- AC:** Located in several locations, including near the center and on the right side.
- GATE:** Located on the left side, labeled "TO SAN JOSE".
- VANT:** Located on the left side, labeled "OAKPORT ST".
- BUILDING:** Located on the right side, labeled "COLISEUM WAY".
- COLISEUM WAY:** A street name located on the right side.
- MONITORING OFFICE:** Located on the right side.
- SODI:** Located on the right side.
- WIRE:** Labels for "WIRE ELEV 0.744" and "WIRE ELEV 1.486" are present.
- EL:** Labels for "ELEV 44.806", "ELEV 44.800", and "ELEV 44.721" are present.
- Match Line:** Labels for "MATCH LINE (SEE PPL3)" and "MATCH LINE (SEE PPL4)" are present.
- Dimensions:** Numerous dimensions are shown as horizontal and vertical offsets, such as 5.75, 5.25, 5.15, 5.00, 4.80, 4.60, 4.40, 4.20, 4.00, 3.80, 3.60, 3.40, 3.20, 3.00, 2.80, 2.60, 2.40, 2.20, 2.00, 1.80, 1.60, 1.40, 1.20, 1.00, 0.80, 0.60, 0.40, 0.20, and 0.00.
- Elevations:** Elevation markers range from N28°45'00"W to N29°38'07"W.

PRELIMINARY INVESTIGATION SECTION

STATE OF CALIFORNIA		DIVISION OF STRUCTURES STRUCTURE DESIGN 14	BRIDGE NO. 33-0040R	HIGH STREET VIADUCT (REPLACE)	
DEPARTMENT OF TRANSPORTATION		STRUCTURE	SECTION 2021	RIGHT BRIDGE FOUNDATION	PLAN NO.
ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN					

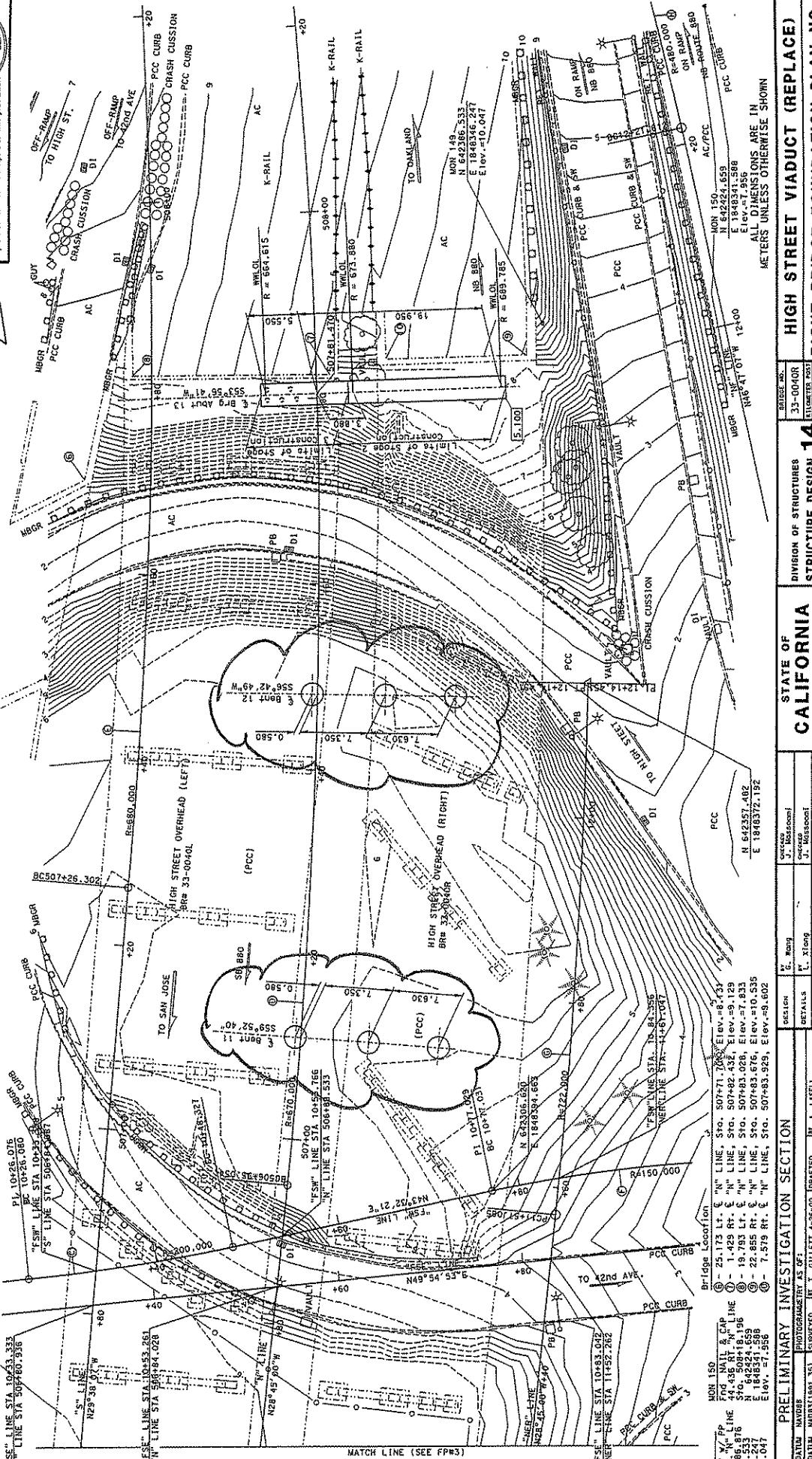
CITY	COUNTY	ROUTE	ELEVATION POINT		SHEET NO.	TOTAL
			ST	FT		
Q1	ALA	880				

REGISTERED CIVIL ENGINEER

PLANS APPROVAL STAMP
 The State of California or the officer or officials
 herein set forth are not responsible for the accuracy
 or completeness of technical details of this plan.
 CIVIL ENGINEER

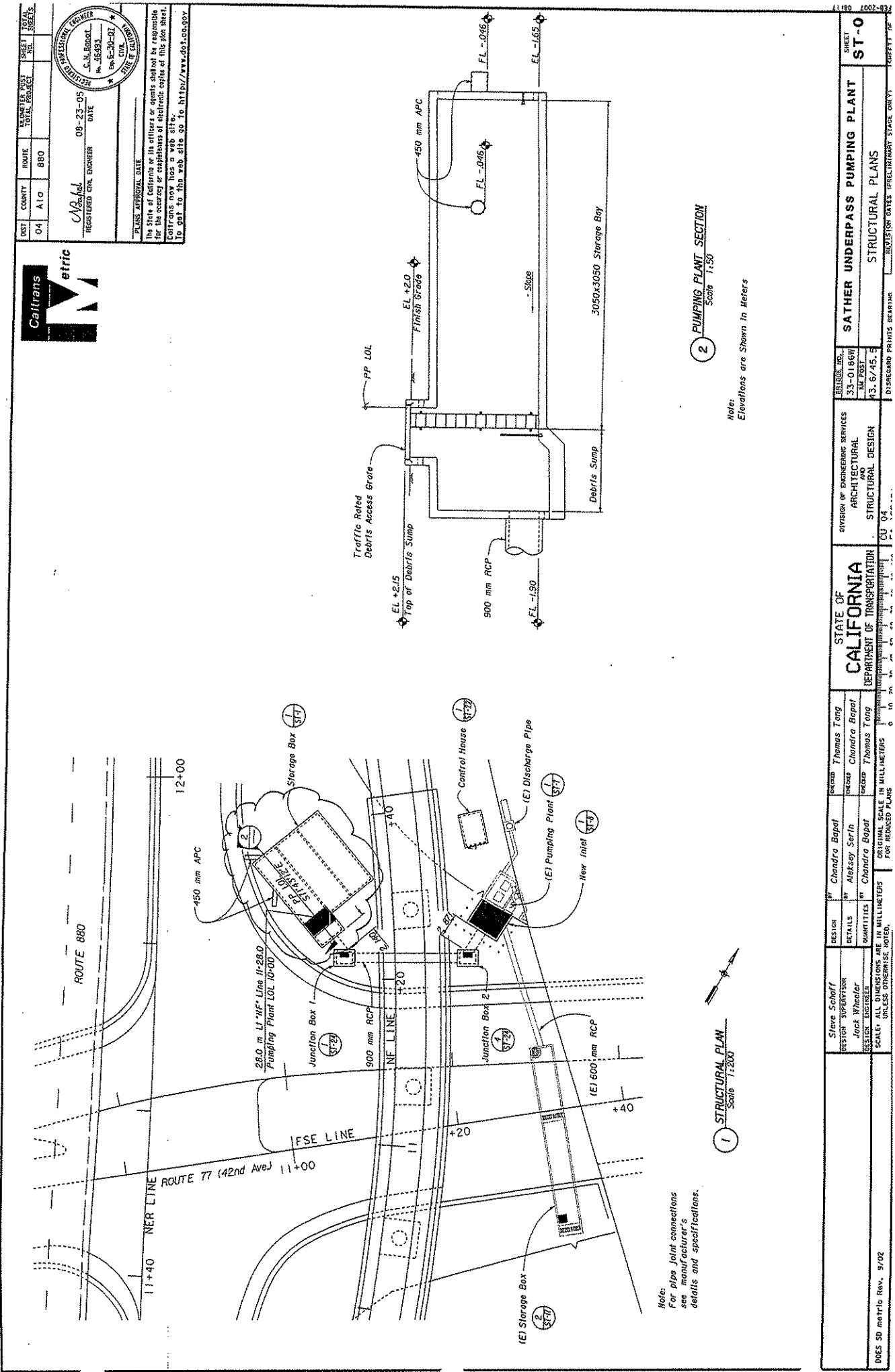
NOTES:

- Not all Piles shown
- Indicates Bottom of footing elevation



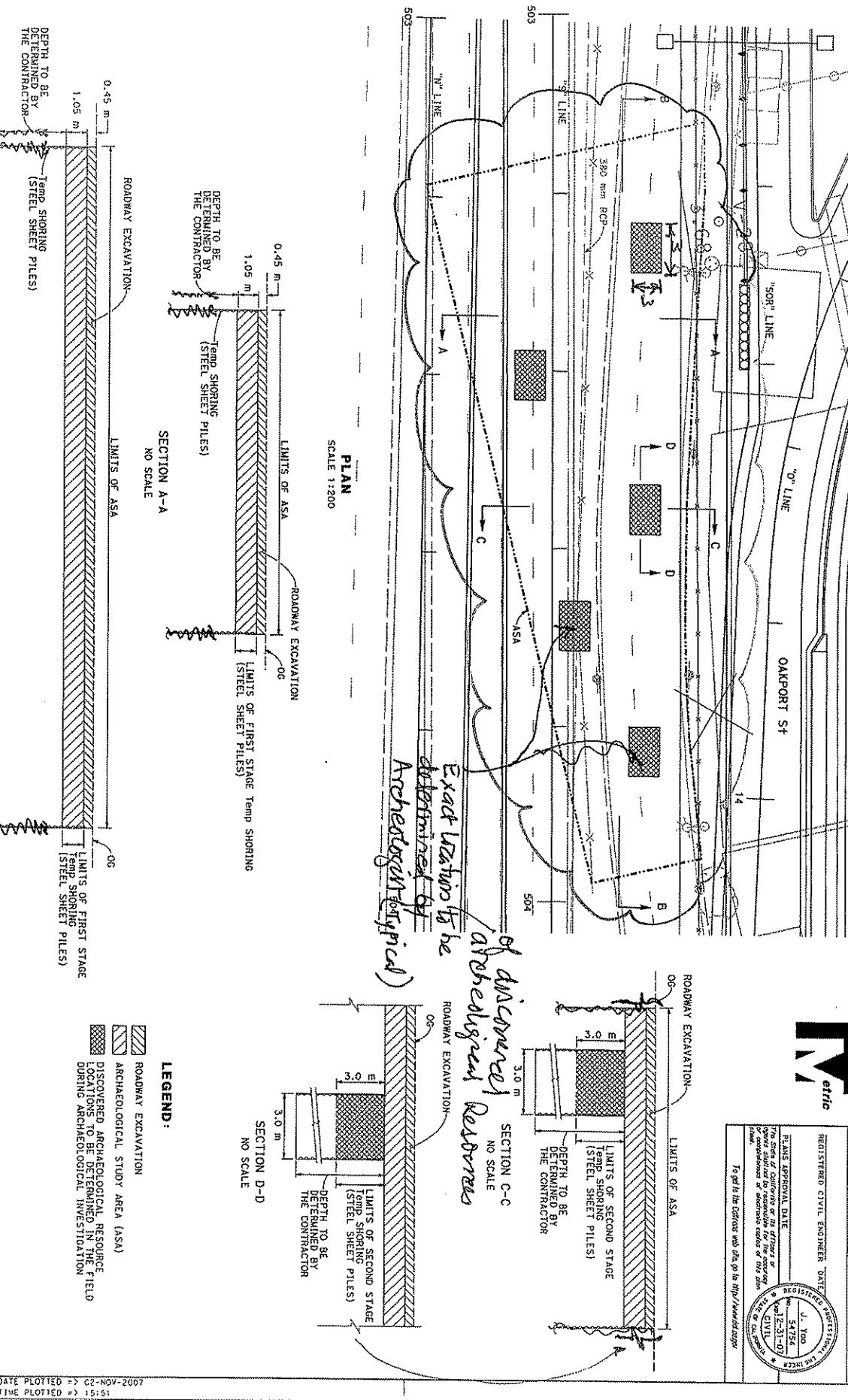
RIGHT BRIDGE FOUNDATION PLAN NO. 1											
JUNIOR ONE SECTION											
13.6-15.41											
ELEVATED WALKWAY BEAMS											
SECTION LINE 1-1											
EAST SIDE OF FOUNDATION											
WEST SIDE OF FOUNDATION											
SOUTH SIDE OF FOUNDATION											
NORTH SIDE OF FOUNDATION											
17											

No.	R	Δ	T	L
(3)	260,000 ..	6°22'23"	11,135	22,246
(4)	610,000	37°27'46"	227,192	438,080
(5)	660,000	36°34'41"	224,743	431,115
(6)	1150,000	12°14'13"	16,079	32,056
(7)	7122,000	4°33'39"	28,698	57,356
(8)	480,000	9°27'48"	39,730	79,279



4. ARCHAEOLOGICAL STUDY AREA PLANS

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION Caltrans	FUNCTIONAL DESIGN	SUPERVISOR ALBERT J. ZEPEDA	CALCULATED/DESIGNED BY DEL TABANCAY	DATE 10/06	REVISED BY JIE YAO	DATE REVISED 10/06
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DIST. COUNTY	SCOTT	ROUTE NUMBER	ROUTE 99	SHR. NO.	ROUTE SHEETS
04	A10	880	43.945.4		
PLANS APPROVAL DATE					
REGISTERED CIVIL ENGINEER - DATE PLANS PREPARED					
J. YAO 5/7/06					
REGISTERED CIVIL ENGINEER - DATE PLANS APPROVED					
J. YAO 5/7/06					
RECEIVED ON DATE APPROVED OR ISSUED OR CONSIDERED FOR APPROVAL OR CONSIDERED AS ACCEPTABLE					
MAY 12-21-07					
CIVIL ENGINEER					
CONTRACTOR					
IN THIS DRAWING THERE ARE NO PLANS APPROVED OR CONSIDERED AS ACCEPTABLE					

5. GENERAL WASTE DISCHARGE REQUIREMENTS

General Waste Discharge Requirements for: Discharge or reuse of extracted and treated groundwater resulting from the cleanup of groundwater polluted by fuel leaks and other related wastes at service stations and similar sites can be found at:

<http://www.waterboards.ca.gov/sanfranciscobay/Agenda/11-13-06/5afinalrevised/ORDER%20NO.%20R2-2006-0075rev.pdf>

6. LIST OF PUBLICLY OWNED TREATMENT WORKS (POTW) FOR
DISPOSAL OF CONTAMINATED GROUND WATER

Alameda POTW

City Discharger	Treatment Plant Name	VDR Discharger Name	Discharger Contact Name	Contact Phone No.	Contact Email	Mail Address	C1 Contact for Groundwater & De-Watering Discharges	Service Area of the POTW
6 Dublin	Dublin San Ramon Service District	Dublin San Ramon SD	Bob Andison/ Levi Fuller	925-875-2360, cell 925-70-4777, 925-846-0568, ext. 119	anderson@dsrsd.com, fuller@dsrsd.com	DsRSRD, 7051 Dublin Blvd, Dublin, CA 94568	Call Env. Compliance Officer Eric Kuehnen @ 925-875-2335 "case-by-case situation - greater than during storms" Testing required, \$385 for annual permit, per million gal fee, etc..	Dublin, San Ramon, & Pleasanton
7 Pleasanton			Richard Lagomarsino, Daniel Smith	931-5399	rlagomarsino@ci.pleasanton.ca.us, dsmith@ci.pleasanton.ca.us	Richard Lagomarsino, Lead Utility Operator and Daniel Smith, Utility Superintendent, 3323 Bush Road, Pleasanton, CA 94568	Same as Dublin-San Ramon SD - see line #A-7	Same as Dublin-San Ramon SD - see line #A-7
8 Union City	Union SD	Union SD	Roger Ham	510-477-7540	roger.ham@ci.unioncity.ca.us	Roger Ham, Collection Service Manager, Union Sanitary District, 3072 Benson Road, Union City, CA 94587	Best contact is Von Henry @ 510-477-7657. USCD would consider if there are no other options available, ie. if storm drain is contaminated using the storm drain is "ok". Call Env. Source Control's - Alex Parets, 925-960-8144. "requires testing, then annual G.W discharge Permit of \$250, and \$6,750 PMG's of discharge." - Will mail packet to Call Ms. Diane Ndeu @ 510-981-7960	Services, Fremont (including Niles), Union City, & Newark
9 Livermore	City of Livermore WPCP	City of Livermore	Darren Greenwood	925-360-8160	darrennewcode@ci.livermore.ca.us	Darren Greenwood, Water Resources Manager, 101 West Jacksonian Blv, Livermore, CA 94551	They will accept discharge with test results. Permit fee is \$470 plus info. See email or 622/2104 has all info. Contact John Camp in Env. Services @ 510-577-8029. "haven't accepted in the past... prefer Baker tanks for sediment, then discharge to storm drain" There is a special Discharge Permit, includes \$240 per 100 cu. ft. Would consider proposals. Best contact Jeff Carlson 510-481-6897.	City of Livermore, the Ruby Hills Development of Pleasanton, and the Veterinarian's Hospital of unincorporated Alameda County.
10 Hayward	City of Hayward WPCP	City of Hayward	Alex Antoci	510-383-4720	alexa@ci.hayward.ca.us	Alex Ameri, Deputy Director/Utilities, Dept. of Public Works, 777 B Street, Hayward, CA 94541-3107	Per Alex Ameri: 90% of the city of Hayward is served by this sewer system - the other 10% (the North end, north of "A" St.) is serviced by Ora Loma Sanitation	
11 San Leandro	San Leandro WPCP	City of San Leandro	Dean Wilson	510-577-6100	dwilson@ci.sanleandro.ca.us	Dean Wilson, Water Pollution Control Plant Manager, 3000 David St., San Leandro, CA 94527	Plant phone # is 510-577-3434 - they only do "the city boundaries" of San Leandro - not the unincorporated areas - it's sort of a Zig-Zag kind of thing... They do have their boundaries on GIS... call Mike Farmer at 517-3339	
12 San Lorenzo	Oro Loma SD	Oro Loma S.D.	Michael C. Cameron	510-481-6969	mcameron@co.alameda.org	Michael Cameron, General Manager, Oro Loma Sanitary District, 2600 Grant Avenue, San Lorenzo, CA 94580	Call Bill Haistead @ 510-481-6863 - he has base maps and shape files which he will make available on CD or pdf. Service area is all of San Lorenzo, parts of San Leandro, Hayward, and Castro Valley, and parts of unincorporated Alameda County. "Ora Loma is a district, and not subject to city boundaries..."	
13 Castro Valley	Castro Valley S.D.	Castro Valley S.D.	Reiland Williams	510-537-0757	reiland@cvsan.org	Reiland Williams, General Manager, Castro Valley Sanitary District, 21640 Marshall Street, Castro Valley, CA 94546-0198	Fee, permit, plan, testing, possible treatment required. Potential problems are large sediments and amounts. May only allow discharge between 2 and 4 A.M. Service area is 40% of both Hayward and San Leandro, San Lorenzo, and some unincorporated Alameda County	
14 Oakland	EBMUD WPCP	EBMUD	Maria A. Bonnarcos; Jennifer Smith	510-287-1141; 510-287-0519	mbonnarcos@ebmud.com; jsmith@ebmud.com	David R. Williams, P.O. Box 2035 (MS#702), Oakland, CA 94623-1155	Web site: www.ebmud.com or call 510-287-1651 "for determination of your permitting needs" Best contact Gail Tupper at 510-287-1608 Permit is 13 pages long (costs \$650) - "every situation is different/special..." Cities of Alameda, Albany, Berkeley, El Cerrito, Emeryville, Kensington, Oakland, and the Siege Sanitary section of Richmond.	
15 Alameda		City of Alameda	Wali Wazni	510-749-2853	wazni@ci.alameda.ca.us	David R. Williams, P.O. Box 2035 (MS#702), Alameda, Alameda Point, Building 1, 3500 West Mall Share, Room 110, Alameda, CA 94501	Same as EBMUD WPCP - see line # A-14	Same as EBMUD see # A-14
16 Albany	City of Albany	Am Chantey		510-228-3768	achantey@ci.albany.ca.org	An Chaney, Director of Community Development and Environmental Resources, City of Albany-City Hall, 1000 San Pablo Ave, Albany, CA 94706	Same as EBMUD WPCP - see line # A-14	Part of EBMUD see # A-14
17 Berkeley	City of Berkeley	Henry Yee		510-981-6303	hyee@ci.berkeley.ca.us	Rene Cardinavus, Public Works Director, City of Berkeley, 2180 Milvia St., Berkeley, CA 94704	Same as EBMUD WPCP - see line # A-14	Part of EBMUD see # A-14
18 Emeryville	City of Emeryville	Maurice Kaufman		510-596-4334	mkaufman@ci.emeryville.ca.us	Hank Van Dyke, City Engineer, City of Emeryville, 133 Park Ave., Emeryville, CA 94608	Same as EBMUD WPCP - see line # A-14	Part of EBMUD see # A-14
19 Oakland	City of Oakland	Fund Stevens; Atien Law		510-238-6607 (L.R.) 523-6929(A.L.)	fsstevens@oaklandnet.com; atienw@ratkam.net.com	Michael Neary, Engineering Division Manager, City of Oakland, 351 Frank Ogawa Plaza, Suite 4314, Oakland, CA 94612	Same as EBMUD WPCP - see line # A-14	Part of EBMUD see # A-14
20 Piedmont		Larry Rosenthal		510-210-3100	lrosenthal@ci.piedmont.ca.us	Larry Rosenthal, Director of Public Works, City of Piedmont, 120 Vista Ave., Piedmont, CA 94611	Same as EBMUD WPCP - see line # A-14	Part of EBMUD see # A-14

7. ALAMEDA COUNTY -POTW SERVICE AREA

Alameda County - POTW Service Areas

